

To: ALL BRIDGE DESIGNERS 02.2

From: Ralph E. Anderson

Subject: Drilled Shaft Policy Walph E. andersan

Date: June 17, 2002

Drilled shafts provide a viable and economical foundation solution in certain conditions. The Department has developed guidelines for appropriate applications of drilled shafts. The Guide Bridge Special Provision for Drilled Shafts (GBSP 2) was recently updated and six new base sheets have been developed which are included herein. The planner and designer should apply these resources on applicable projects. GBSP 2 and the English and metric versions of these new base sheets may be found on the IDOT web site.

Bridge planners must consider many issues in addition to design feasibility and construction costs before selecting drilled shafts as the most appropriate foundation support. Drilled shafts may be used to address vertical and lateral pile capacity concerns resulting from large scour depths, potential liquefaction, low soil strengths and inadequate pile embedment. Drilled shafts may also be used at sites indicating large variations in the top of rock elevations to avoid spread footing steps or construction changes in footing elevation. Concerns about pile driving vibration, noise or overhead clearance have also been reasons for specifying drilled shafts. In some locations they can also eliminate the need for cofferdams, seal coat and structure excavation.

A critical piece of information required for planning and construction of drilled shaft piers at stream crossings is the Estimated Water Surface Elevation (EWSE). This is the typical water surface elevation estimated to be prevailing at the time of construction, and is to be shown on the TSL Plans and Final Design Plans. Obviously, knowing when construction will actually take place and predicting the water surface elevation two or three years in advance of construction is a monumental if not impossible task. However, a "best effort" is necessary, and it should be recognized that the EWSE will at times be subject to many factors which could render it inaccurate. The attached base sheets contain a note, which allows for adjustment to the plans when the prevailing water surface is consistently different from the EWSE. The expectation is that if 50% of the drilled shaft projects can avoid the "adjustments" allowed, it will be an improvement over our current situation, which gives no direction to the contractor as to what water elevation may be expected.

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Many bridge sites will be located in controlled pools, especially on major rivers, where the normal pool elevation established by the United States Corps of Engineers or other agencies will be readily available and serves as a very accurate water surface elevation. Other sites will be located at or near a United States Geological Survey stream gage station, which may be a source of data for estimating or verifying a typical water surface elevation. However, many sites will require an estimate based on hydraulic site surveys. In this case a standard method of finding the EWSE is presented in the attached sheet titled "Estimated Water Surface Elevation". This method is to be used only when better information/data is not available. A major assumption of any method, including the standard method, is that all construction will take place in the month of April, building some conservatism into the estimate.

The Bureau of Bridges & Structures Hydraulic Unit will record the stream site existing water surface elevation, date of survey and top of bank elevation in their Hydraulic Report review comments for all potential drilled shaft projects, for easy reference. It is recommended that this procedure also be followed on state owned bridges requiring a preliminary bridge design and hydraulic report prepared by others for local agencies.

The attached base sheets include various pier types and one for abutment details. Correct pier type selection is important to address constructability issues, and the following guidance is offered to assist in that selection:

- Open Column Drilled Shaft Pier: (Base Sheet P-DS) This substructure type typically provides the most economical shaft alternative where stream conditions permit. The top of the drilled shaft should be located 300 mm (1 ft) above the EWSE, which should be shown on the TSL and final plans. If aesthetics allow, permanent casing may be specified to simplify construction of the shaft through the water. If the appearance of permanent casing is undesirable, the length of the shaft where casing will not be allowed to remain in place shall be designated on the plans. For constructability reasons, that length should typically not exceed 3 m (10 ft). If the shaft extends through water deeper than 3 m (10 ft), permanent casing should be specified to make up the difference. Although this base sheet is detailed for a pier located in water where no permanent casing is permitted, permanent casing can be added or the base sheet modified for use at piers without concerns for water such as overbank piers or grade separations. As with any of the pier types, when permanent casing is necessary, the minimum limits should be shown on the plans and a separate pay item, Permanent Casing, should be added.
- Column-Web Wall Drilled Shaft Pier: (Base Sheet P-DSWW) Waterways
  with a history of debris collection or ice jams may necessitate the use of a
  web wall between the shafts. The need for this wall must be carefully
  evaluated and only used when conditions warrant since it adds cost and

complexity to the project. The use of this pier type without a cofferdam is limited to locations where less than 1.8 m (6 ft) of water is expected at the shaft location. Construction of the web wall has been an issue in the past and thus the base sheet provides a construction sequence and a pay item "Underwater Structure Excavation Protection" for this work. Since the lower web wall is only connected to the upper web wall (not the shafts), the upper web wall should extend to 1.8 m (6 ft.) above the lower web wall or to the project's Design High Water Elevation whichever is higher. In cases where the top of the upper web wall is within 2.13 m (7 ft.) from the bottom of the pier cap, we recommend the upper web wall be extended to the bottom of cap.

- Encased Drilled Shaft Pier: (Base Sheet P-DSSW) This pier type may be used if dictated by watercraft traffic requiring a flush crash wall, or if an aesthetic requirement is needed to match the existing or new substructures, etc. The permanent casing will be covered by the encasement wall and thus is not an aesthetic concern. The drilled shaft diameter must be shown at least 300 mm (1 ft.) less than the encasement width to accommodate shaft construction tolerances. Since the encasement width limits the shaft diameter, more shafts are normally required, which causes this shaft supported pier type to be the most expensive. The use of this pier type without a cofferdam is limited to locations where less than 1.8 m (6 ft) of water is expected at the shaft location. This wall construction differs from the web walls in that the forms, reinforcement cage and concrete tremie pour completely surround the shafts and the upper encasement wall is poured monolithically with the column cage. The construction sequence of the encasement wall has been an issue in the past and thus the base sheet provides a construction sequence and a pay item "Underwater Structure Excavation Protection" for this work.
- <u>Drilled Shaft Pier with Transfer Beam:</u> (Base Sheet P-DSTB) This pier type is most suitable when the design loading (vessel impact, ice, seismic, etc.) requires more strength, stiffness, and redundancy along the axis of the pier. The transfer beam also provides additional construction tolerance to incorporate out of location shafts which are more likely in deep water shaft installations. Permanent casing can avoid the need for a cofferdam, provide a form through deeper water sites and add protection against stream abrasion. However, since the casings will remain below the beam, aesthetics and debris collection should be considered.
- <u>Drilled Shaft Pier with Crash Wall:</u> (Base Sheet P-DSCW) This pier type is normally used at grade separations where the proximity of the adjacent roadway or railroad traffic dictates the use of a crash wall. Since the crash wall is not acting as a footing, it can typically extend just 600 mm (2 ft)

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below the finished grade (similar to the abutment). The crash wall pier can also be used in locations requiring added strength, stiffness, and redundancy along the axis of the pier. In cases where the shaft diameter causes the crash wall width to increase excessively, a wider grade beam may be located below the thinner crash wall to connect it to the larger shafts.

• Abutment Drilled Shaft Details: (Base Sheet A-1-DSD) This base sheet may be used in conjunction with any of the above pier applications or to support single span structures. At sites where drilled shaft support is required at one abutment or at least half the substructure units, consideration should be given to using shafts at the remaining substructures to lower the unit shaft cost, when the cost advantage of using alternative foundation support is not significant.

Other issues related to the base sheets include:

- The spiral reinforcement in the shaft is shown at a 150 mm (6 in.) pitch to promote unrestricted flow of the concrete during the variety of difficult installation conditions present which could otherwise lead to construction defects. As such, the drilled shaft shall be designed as a column with ties (or hoops) spaced at 150 mm (6 in.) centers.
- The drilled shaft diameter is 150 mm (6 in.) larger in soil than in rock. However, they both use the same diameter reinforcement cage. This results in a 50 mm (2 in.) concrete cover for the reinforcement in rock and 125 mm (5 in.) of concrete cover for the reinforcement in soil. This ensures the proper rebar cover in soil regardless of the installation procedure and reduces the need for contractors to oversize the shaft in soil to drill the rock. At piers with columns directly above the shafts, the columns are detailed 150 mm (6 in.) smaller in diameter than the shafts to allow for construction tolerance in the shaft's plan location while enabling the designer to use the same diameter cage in the column and shaft.

WMK/bb23747

## **ESTIMATED WATER SURFACE ELEVATION**

(EWSE)

## Standard Estimating Method

- 1) From Hydraulic Report stream survey find the *existing water surface elevation*, as provided per Drainage Manual 2-601.2 & Fig. 2-601.2 b, (or low flow) at the bridge site and the month that this elevation was surveyed. Also, find the top of bank elevation from the stream cross sections at the bridge.
- 2) The *existing water surface elevation* is assumed to be a "typical low flow", in any year, for the month taken.
- 3) April is assumed to be the typical "high" month for water surface elevations and September is assumed to be the typical "low" month.
- 4) Using an equal monthly increment of 0.75, add or subtract from the *existing water surface elevation*, going from the month in step 1 to the month of construction (usually assumed to be April), within a calendar year. See example below.
- 5) The maximum elevation to be used is 75% of the difference from the typical September low flow elevation to the top of bank elevation added to the September low flow elevation.
- 6) The Estimated Water Surface Elevation is the lower elevation from step 4 or step 5.

## **Example**

From Hydraulic Report stream cross section or profile: *Existing water surface elevation* = 606.1 at bridge site, date of survey is November 1999.

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Nov. Oct. Sept. Aug. July June May April 606.1 -0.75 -0.75 +0.75 +0.75 +0.75 +0.75 = 608.35
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Check maximum: Top of bank elevation at bridge site is 611.3 Typical low flow for Sept. is 606.1 - 0.75 - 0.75 = 604.6 (611.3 - 604.6) x 0.75 + 604.6 = 609.6; 609.6 > 608.35

Therefore EWSE = 608.35























